Nanotechnology and Oxidative Techniques for Remediation

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Presentation Overview

- Introduction to Oxidative and Reductive technologies for TCE and PCB removal (D. Bhattacharyya)
- Overview of reductive dechlorination involving bimetallic nanosystems (**D. Meyer**)
- Summary of laboratory studies involving Oxidation of TCE (S. Lewis)
- Concluding Remarks

Removal of TCE at Ambient Temperature

Reductive Dechlorination of TCE

Nanosiled Netals

 $(nano)Fe^{0} + TCE \rightarrow Fe^{2+} + Ethane + 3Cl^{-}$ $(Bulk)Fe^{0} + TCE \rightarrow Fe^{2+} + intermediates$ $+ nCl^{-}$

Systems Used:

Zerovalent metals (**Fe**), Bimetallic systems (**Fe/Pd, Fe/Ni**), Supported Platforms

Oxidative Destruction of TCE

For oxy Radical

TCE + **OH** \rightarrow **CO**₂, **Organic Acids**

Systems Used: Standard Fenton Reaction, Modified Fenton Reaction using nontoxic chelate (citrate, gluconic acid) (L) as a chelating agent (FeL).

Background (reductive dechlorination at room temperature)



TCE Dechlorination by Membrane-based Bimetallic Nanoparticles



Longevity of Fe/Ni Nanoparticle Reactivity

Dechlorination of Polychlorinated Biphenyls (PCBs)





PCB 77 (3,3',4,4') dechlorination by membrane based Fe/Pd (Pd=2.3 wt%) nanoparticles at room temperature

Technology Enhancement: On-site Generation of Chelate and H₂O₂

HYPOTHESIS

Gluconic acid produced by enzymatic reaction would act as a chelate in Fenton reaction, and thus allow degradation of TCE & PCBs near neutral pH



The Initial Rate of Glucose Oxidation Measured by H₂O₂ Formation at Different Substrate Concentrations



Groundwater Remediation Using Combined Strategies For Reduction and Oxidation



TCE Reduction Using Fe/Pd Nanoparticles

-Batch Studies of Matrix Effects

- Packed Column (Gravel) Studies
 - In-Situ Injection Implications



Reductive Dechlorination: Hydrogenolysis and Bimetallic Systems

 A catalyzed Hydrogenolysis mechanism is believed to exist for bimetallic ZVM systems.



• This mechanism is supported by the fact that dechlorination rates increase as the H-promoting ability of the 2nd metal increases:

 $k_{\text{Pt/Fe}} > k_{\text{Pd/Fe}} > k_{\text{Ni/Fe}} > k_{\text{Fe}}$

Batch Cycle Study for TCE Degradation by Ni/Fe (Ni = 20 wt%) Nanoparticles in Deoxygenated Water with Headspace:

Metal Loading = 2.5 g/L; pH = 6.5; $TCE_0 = 10 \text{ mg/L}$



Aspects to Address for Successful TCE Dechlorination Using Direct Injection of Bimetallic Nanoparticle Systems

- What composition and metal loading are necessary for rapid and efficient TCE dechlorination? (batch data)
- Will the presence of non-chlorinated chemical species present in Paducah groundwater and soil alter the performance of Fe-based nanoparticle dechlorination systems? (batch and column experimental data)
- What impact, if any, will dissolved oxygen have on dechlorination kinetics? (batch data)
- What type of **mobility** will **nanoparticles** have while moving within plumes? (theoretical modeling)

Dechlorination of TCE Using Fe/Pd Nanoparticles (1 wt% Pd) In Deoxygenated Water with Headspace:

Metal Loading = 1.0 g/L; pH = 6; $C_0 = 16.6$ mg/L TCE



Dechlorination of TCE in Deoxygenated Paducah Water Using Fe/Pd Nanoparticles with Variable Metal Conditions:

 $C_0 = 20.5 \text{ mg/L}; \text{ pH} = 5$



Reduction of a 20 ppm TCE Solution in Paducah Water Under Aerobic Conditions Using Fe Nanoparticles Post-Coated With 0.5 wt% Pd



Dechlorination of TCE Using Fe/Pd Nanoparticles (1 wt% Pd) In Paducah Water with Gravel:

pH = 6; $C_0 = 21.9 \text{ mg/L TCE}$, Reaction time = 0.5 hr



Packed Column Studies for Simulated Groundwater Injection



Packed Column Studies:

Flowrate = 73 ft/day; Metal Loading = 0.23 g/L Fe/Pd (0.5 wt%); $C_0 = 25 \text{ ppm TCE}$; pH =7.0



Packed Column Studies:

Flowrate = 82 ft/day; Metal Loading = 0.46 g/L Fe/Pd (0.5 wt%); $C_0 = 25 \text{ ppm TCE}$; pH =7.0



Examination of Material Usuage for the Reduction of 400 ppb TCE Using Fe/Pd Nanoparticles

Time Basis	24	h	k _{SA}	1.30E-01	L.m ⁻² .h ⁻¹ (Fe +	0.5 wt% Pd)			
Treatment Diameter	400	ft	Fe/Pd loading	0.25	g/L				
Treatment Depth	20	ft	mass Fe/Pd	9,433	g/h = 20.75	3 lbs/h			
Asssumed Porosity	0.4		Surface Area	30	m ² metal/g				
Treatment Area	125,664	ft ²	Loading	7.5	m ² metal/L				
Treatment Volume	2,513,274	ft ³							
Treatment C.S. Area	3,200	ft ²	TCE	400	ppb				
Groundwater Velocity	10	ft/day							
	0.42	ft/hr	С _{тсе} @ 1h	0.000	ppb				
Volume per hour	1,333	ft ³ /h	TCE reacted	1.15E-01	moles/h				
	37,733	L/h							
	Fe:T	CE ratio	4:1						
r	noles Fe co	nsumed	4.59E-01						
mass Fe consumed Fe remaining		25.66 0.056 9,407.67 20.697	g/h Ibs/h g/h <mark>Ibs/h unus</mark>	sed					
Note: one can treat 38000 liters of water with 26 g of nano Fe particles									

TCE Oxidation by Chelate-Based Modified Fenton Reaction

-Role of Surfactant Study -Effect of Gravel on Reactivity -H₂O₂ Decomposition by Ferrous and Ferric Iron



Why Chelate-Based Modified Fenton's Reaction?

- Controlled release of Fe²⁺
- Prevent Fe(II) oxidation
- At near neutral pH, prevent Fe(OH)₃ precipitate by complexing with Fe(III)
- Have a better H_2O_2 utilization during the reaction
- Hydroxy radical and superoxide* radical formation near neutral pH operation
- Potential biodegradation enhancement
- Chelate can also be immobilized in nano-particles

*Superoxide Radical Formation:OH • $+H_2O_2 \rightarrow H_2O + HO_2 \bullet$ $HO_2 \bullet \rightarrow H^+ + O_2 \bullet^-$

Required Materials for Chelate-Based Modified Fenton Reaction

Citrate

Ferrous Sulfate

Hydrogen Peroxide



http://www.hort.purdue.edu/ext/senior/ fruits/orange1.htm



http://www.drugstore.com/popups/largerphoto/def ault.asp?pid=77653&catid=39521&size=300&trx =29888&trxp1=77653&trxp2=1



http://pics.drugstore.com/prodimg/738 64/200.jpg

Iron-Citrate Species Distribution



TCE Degradation as a Function of Peroxide Consumed for Varying Citrate (L)-to-Fe Ratios Showing the Potential Reduction in Peroxide Needs for Chelate-Based Systems



Effect of Dissolved Oxygen for TCP Oxidation by Fe²⁺ + PAA + H₂O₂ System (chelate modified system)



Effect of Gravel on TCE Destruction Using Chelate-Based Modified Fenton Reaction

TCE destruction model as a function of time for TCE:Fe:Citrate: H_2O_2 molar ratio of 1:1:1:8. Initial TCE concentration of 100ppm. Initial pH = 7.



Chelate-Based Modified Fenton Reaction (pH=7.0) Using Paducah Water With Varying Fe(II):H₂O₂ Ratio



Packed Column Studies for Simulated Groundwater Injection



The Challenges of DNAPL

1.) TCE droplets dispersed in the aqueous phase will act as a source of TCE and shrink as mass is lost to the aqueous phase. The mass transfer between phases may have substantial impact on the observed reaction time for both oxidation and reduction.



2.) If DNAPL droplets are dispersed within soil and rock, they may require much greater reaction times for direct treatment. To overcome this problem, surfactant addition can potentially be used to mobilize the DNAPL from the sediment. Laboratory packed columns operating under trickle-flow can be used to examine this phenomenon.



Dispersed DNAPL Droplets



DNAPL Extraction using surfactant injections



Dispersed DNAPL Droplets

Chelate-Modified Fenton Reaction (initial pH=7.0, no further adjustments made) Using DIUF Water with DNAPL (2000ppm TCE) and Varying Fe(II):H₂O₂ Molar Ratio



Effect of Surfactant for TCE Dechlorination by Fe^{2+} + Citrate + H_2O_2



Chloride Formation from TCE Dechlorination with and without Surfactant



Chloride Formation During CCl₄ dechlorination under Standard and Chelate-Based Modified Fenton Reaction at 24 hr Reaction Time (role of superoxide radical)



Ref: Li, Bachas, and Bhattacharyya, I&EC Res (2007)

The Predicted Profiles of superoxide [O₂-] for the Standard and Chelate-Based Modified Fenton Reactions



Ref: Li, Bachas, and Bhattacharyya, I&EC Res (2007)

Literature Results for Field Testing of Oxidative and Reductive Treatment Technologies

Site	Area	Agent	Initial TCE, Final TCE	# Injection Wells	Cost
Westinghouse Savannah River	50 ft x 50 ft (depth: ~110-140 ft)	Fe(II)/H ₂ O ₂	21, <mark>0.07</mark> (mg/L)	4	\$511K
Anniston Army Depot	2 acres (depth: ~8-26 ft)	Fe(II)/H ₂ O ₂	1760, Below detection (mg/L)	255	\$5,700K
Trenton, NJ Manufacturing Company*	15 ft x 10 ft (20 ft depth)	Nanoscale Fe ⁰ /Pd	0.445-0.800, 0.016- 0.028** (mg/L)	1	NA

*Pilot test; site contained up to 4600 μ g/L of PCE, DCE (cis and 1,1), VC, Chloroform, and Carbon Tetrachloride

** Values represent maximum removal achieved during initial injection period. Particles injections were reduced as part of testing to observe plume recovery.

Conclusions

- Chlorinated organic destruction in modified Fenton reaction is same for both aerobic and anaerobic conditions
- Water from the Paducah area produces lower TCE destruction rates than deionized water due to the presence of hydroxyl scavengers (near neutral pH operation); will need slightly higher H2O2
- The complete dechlorination of TCE using Fe/Pd (1 wt% Pd) can be achieved in under 30 minutes using a metal loading of 1 g/L (or less) and is not affected by the presence of background chemicals in Paducah water.
- Batch dechlorination results obtained in the presence of Paducah gravel showed >70 % TCE removal in 1 h for 21.0 mg/L TCE using 0.5-1.0 g/L Fe/Pd (0.5 wt% Pd).
- Results for reductive dechlorination under aerobic conditions suggests that the presence of O₂ has minimal impact for the Pd-protected Fe nanoparticles.
- Both oxidative and nanotechnology-based treatments of TCE in a simulated groundwater column demonstrated > 50% TCE removal using minimal chemical dosing.

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